

Radiosity

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References

1. *Computer Graphics: Principles and Practice* -- Foley and Van Dam
Chapter 16, Section 13, Pages 793-806.
2. *Global Illumination* -- Sillion and Puech, Chapters 2–4.
3. *Examining Radiosity* -- Siggraph Course Notes 1993
<http://www.education.siggraph.org/slides/slides93/53_93.htm>
4. *Radiosity* -- Allen Martin
<http://www.cs.wpi.edu/~matt/courses/cs563/talks/radiosity.html>
5. *Graphics Gems I–V*.

Comparison

Ray Tracing

Point Light Sources

Diffuse and Specular Reflection

Sharp Shadows

Weak Model for Ambient Light

Radiosity

Ambient Light

Diffuse Reflection

Soft Shadows

Models Emitters and Reflectors

Diffuse Reflection

Lambert's Law -- $I = I_p k_d \cos \theta$

- I = reflected intensity
- I_p = intensity of light source
- k_d = diffuse reflection coefficient $0 \leq k_d \leq 1$
- θ = direction between surface normal (N) and vector to light source (L)
- $\cos \theta = N \bullet L$
 - N = unit normal to surface
 - L = direction to light source

Observations

- Diffuse reflection is the same in all directions
- Actually 3 equations -- one for each primary color (RGB).

Diffuse Reflection

Formula

$$I = I_p k_d \cos(\theta) = I_p k_d (L \cdot N)$$

I_p = intensity of point light source at infinity

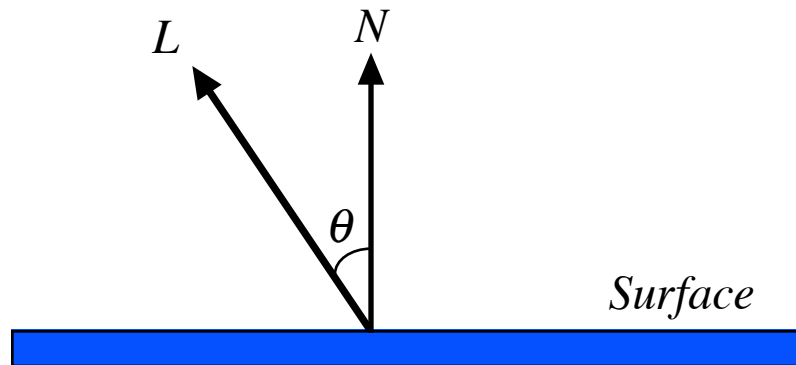
k_d = diffuse reflection coefficient

k_d is a material property

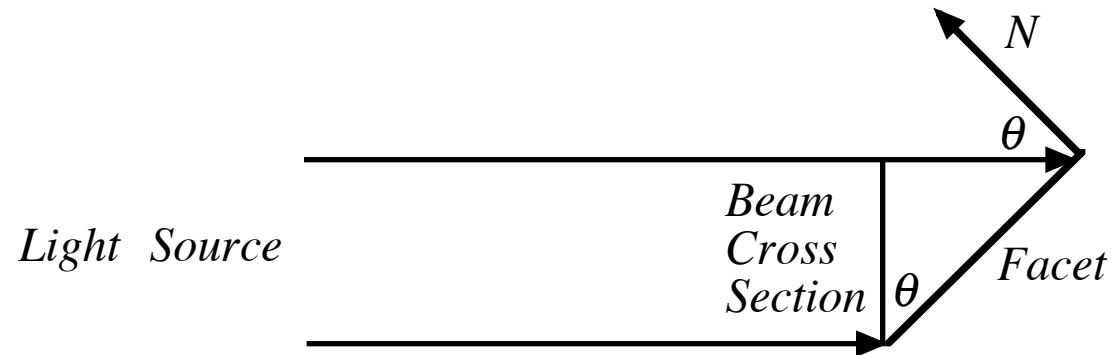
$$0 \leq k_d \leq 1$$

θ = angle between surface normal (N) and direction (L) to point light source

$$\cos(\theta) = L \cdot N$$



Lambert's Law



$$I_{\text{facet}} = \frac{\text{Light}}{\text{Unit Area}} = \frac{\text{Beam Cross Section}}{\text{Facet Area}} \times I_{\text{source}}$$

$$\frac{\text{Beam Cross Section}}{\text{Facet Area}} = \cos(\theta)$$

$$I_{\text{facet}} = \cos(\theta) I_{\text{source}}$$

Radiosity

- Radiosity = rate at which light energy leaves a surface = Power/Area
- Radiosity = emission + reflection
- Radiosity \equiv Intensity($\times\pi$) {Intensity=Radiance=Power/Area/SAngle}
- Radiosity replaces: ambient intensity + diffuse intensity
- **RADIOSITY IS VIEW INDEPENDENT**
- View dependent calculations only for hidden surfaces
- Historically an Energy transfer method based on Heat transfer

Rendering Equation

Energy Conservation

- Total Illumination = Emitted Energy + Reflected Energy
- $I(x, x') = E(x, x') + \int_S \rho(x, x', x'') I(x', x'') dx''$
 - $I(x, x')$ = energy passing from x' to x
 - $E(x, x')$ = energy emitted directly from x' to x
 - $\rho(x, x', x'')$ = reflection coefficient

Remark

- This is precisely the set up for recursive ray tracing!

Radiosity Equation -- Continuous Form

Radiosity = Emitted Energy + Reflected Energy

$$B(x) = E(x) + \rho_d(x) \int_S B(y) \frac{\cos\theta \cos\theta'}{\pi r^2} V(x,y) dy$$

$B(x)$ = radiosity at x -- identified with intensity (or energy)
(total power leaving a surface/unit area/solid angle)

$E(x)$ = energy emitted directly from a point x
(uniform in all directions -- diffuse emitter)

$\rho_d(x)$ = diffuse reflection coefficient -- $0 \leq \rho_d(x) \leq 1$

$V(x,y)$ = visibility term = 0 if x not visible from y
= 1 if x is visible from y

θ = angle between surface normal (N) at x and (light) ray (L) to y

θ' = angle between surface normal (N') at y and (light) ray (L) to x

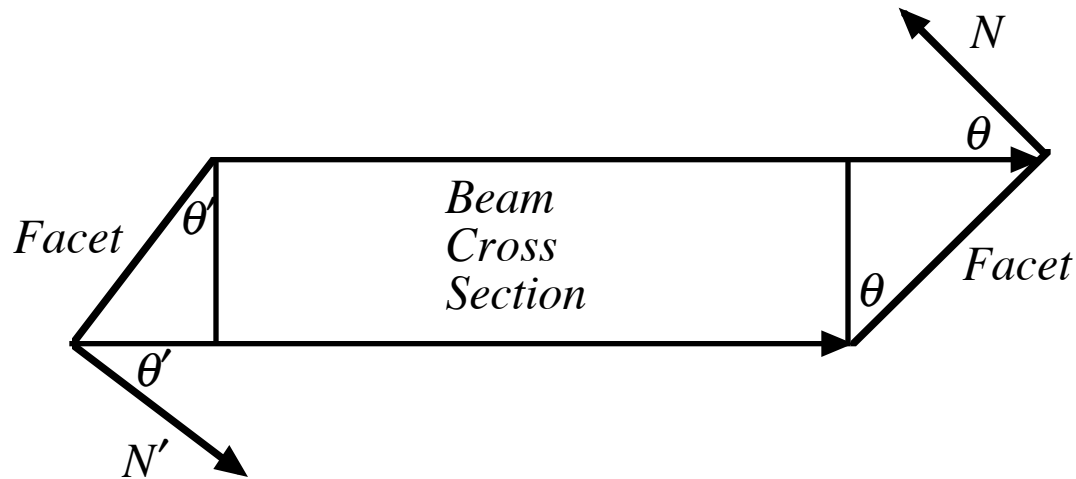
r = distance from x to y -- inverse square law

Radiosity Equation -- Continuous Form (continued)

Reflected Energy

- $\int_S B(y) \frac{\cos \theta \cos \theta'}{\pi r^2} V(x, y) dy = \text{energy reaching } x \text{ from all other } y$
- $\rho_d(x) \int_S B(y) \frac{\cos \theta \cos \theta'}{\pi r^2} V(x, y) dy = \text{energy reflected from } x$
- Note $\cos \theta, \cos \theta'$ from Lambert's Law -- projection of flux onto surface.
- The factor $1/r^2$ comes from inverse square law
- Note mysterious factor of π in denominator.
 - Maps bidirectional flux to usual diffuse reflection coefficient.
(See Sillion, page 14.)
 - Divide all reflection coefficients by π -- rescaling

Lambert's Law



$$I_{\text{facet}} = \frac{\text{Light Deposited}}{\text{Unit Area}} = \frac{\text{Beam Cross Section}}{\text{Facet Area}} \times I_{\text{source}}$$

$$I_{\text{source}} = \frac{\text{Light Emitted}}{\text{Unit Area}} = \frac{\text{Beam Cross Section}}{\text{Facet Area}} \times I_{\text{emitter}}$$

$$\frac{\text{Beam Cross Section}}{\text{Facet Area}} = \cos(\theta), \cos(\theta')$$

$$I_{\text{facet}} = \cos(\theta) \cos(\theta') I_{\text{emitter}}$$

The Radiosity Equation

Radiosity Equation

$$B(x) = E(x) + \rho_d(x) \int_S B(y) \frac{\cos\theta \cos\theta'}{\pi r^2} V(x,y) dy$$

Problem

- Difficult to solve Radiosity Equation because
 - Integral Equation
 - $B(u)$ appears on both sides of the equation!
 - Must know $B(u)$ to find $B(u)$!
- Actually 3 equations -- one for each primary color (RGB).

Solution

- Assume radiosity constant over a small patch
- Break the scene into small discrete patches

Solving the Radiosity Equation

Radiosity = Emitted Energy + Reflected Energy

$$B(x) = E(x) + \rho_d(x) \int_S B(y) \frac{\cos\theta \cos\theta'}{\pi r^2} V(x,y) dy$$

$$B(x) = E(x) + \rho_d(x) \sum_{j=1}^N B_j \int_{P_j} \frac{\cos\theta \cos\theta'}{\pi r^2} V(x,y) dA_j \quad (*)$$

Get radiosity and energy of single patch as area weighted averages

$$B_i = (1/A_i) \int_{P_i} B(x) dA_i$$

$$E_i = (1/A_i) \int_{P_i} E(x) dA_i$$

Integrate discrete equation () to obtain*

$$B_i = E_i + \rho_i \sum_{j=1}^N B_j (1/A_i) \int_{P_i} \int_{P_j} \frac{\cos\theta \cos\theta'}{\pi r^2} V(x,y) dA_i dA_j$$

Radiosity Equation -- Discrete Form

$$B_i = E_i + \rho_i \sum_{j=1}^N F_{ij} B_j \quad i = 1, \dots, N$$

B_i = radiosity on patch P_i -- identified with intensity

E_i = energy emitted from patch P_i

(uniform in all directions -- diffuse emitter)

F_{ij} = form factor -- depends only on geometry, color independent

ρ_i = diffuse reflection coefficient for patch P_i -- $0 \leq \rho_i \leq 1$

$\sum_{j=1}^N F_{ij} B_j$ = energy reaching patch P_i from all other patches

$\rho_i \sum_{j=1}^N F_{ij} B_j$ = energy reflected from patch P_i

Actually 3 sets of equations -- one for each primary color (RGB).

Form Factors

F_{ij} = fraction of energy leaving patch P_i arriving at patch P_j

Theorem:
$$F_{ij} = (1/A_i) \int_{P_i} \int_{P_j} \frac{\cos \theta \cos \theta'}{\pi r^2} V(x,y) dA_i dA_j$$

Proof:

- B_{ij} = radiosity transferred from P_i to $P_j = F_{ji} B_i$
- B_i = energy radiated from P_i per unit area
- $A_j B_{ij}$ = total energy transferred from P_i to $P_j = A_j F_{ji} B_i$

But

$$A_j F_{ji} = \int_{P_i} \int_{P_j} \frac{\cos \theta \cos \theta'}{\pi r^2(x,y)} V(x,y) dA_j dA_i = A_i F_{ij}.$$

Therefore

$$A_j B_{ij} = A_i B_i F_{ij}$$

so

$$F_{ij} = \frac{A_j B_{ij}}{A_i B_i} = \frac{\text{total energy transferred from } P_i \text{ to } P_j}{\text{the total energy radiated from } P_i}$$

Properties of Form Factors

1. *Reciprocity*

$$A_i F_{ij} = A_j F_{ji} \quad \left(= \int_{P_i} \int_{P_j} \frac{\cos \theta \cos \theta'}{\pi r^2} V(x, y) dA_i dA_j \right)$$

2. *Additivity*

$$F_{i, j \cup k} = F_{i, j} + F_{i, k}$$

3. *Partition of Unity (Conservation of Energy)*

$$\sum_j F_{ij} = 1$$

Geometric Interpretation of Form Factors

(Look at 2-D projections first -- project onto a circle)

1. *Point Form Factor*

$$F_{ij} = (1/A_i) \int_{P_j} \int_{P_i} \frac{\cos \theta \cos \theta'}{\pi r^2} V(x,y) dA_i dA_j$$

$$F_{di,j} = (1/dA_i) \int_{P_j} \int_{P_i} \frac{\cos \theta \cos \theta'}{\pi r^2} V(x,y) dA_i dA_j = \int_{P_j} \frac{\cos \theta \cos \theta'}{\pi r^2} V(x,y) dA_j$$

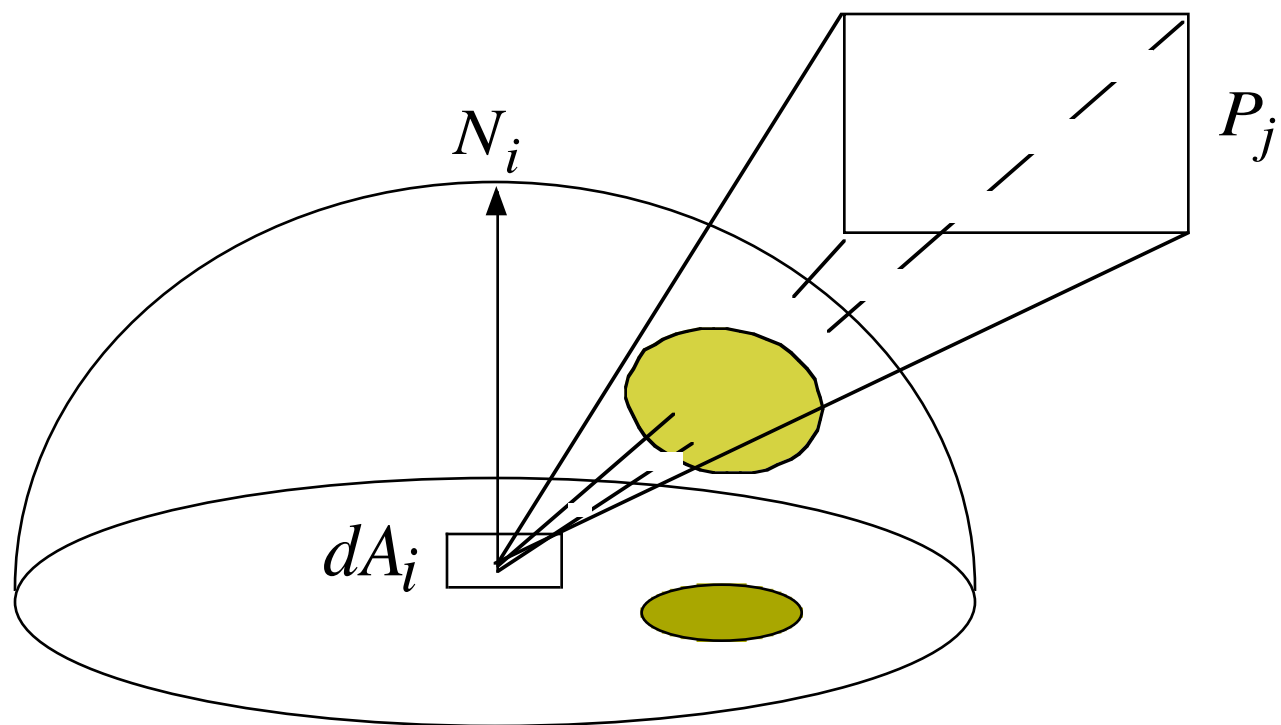
2. *Area Projections*

- Onto Unit Hemi-Sphere -- $\frac{\cos \theta'}{r^2}$
- Onto Base of Hemi-Sphere -- $\cos \theta$

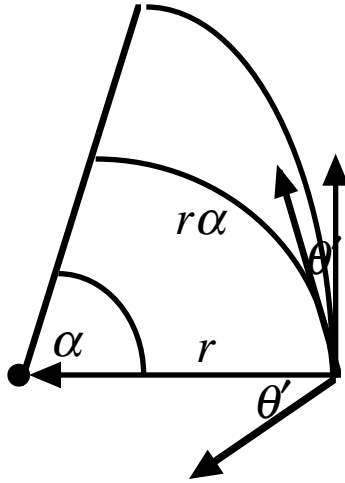
3. *Area of Base of Unit Hemi-Sphere = π*

4. *Note: Equal projections imply equal form factors*

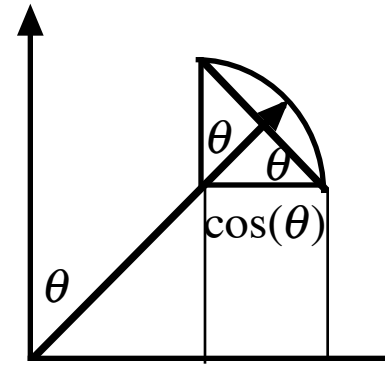
Projections onto a Base of Hemisphere



Projections onto a Circle



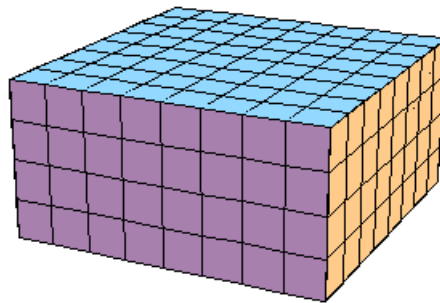
Central Projection
Multiply by $\cos(\theta') / r$



Projection onto x-Axis
Multiply by $\cos(\theta)$

Hemi-Cubes

- Upper half unit cube (side=2) centered at a small patch A_i
- Projection on hemi-cube \equiv projection onto unit hemi-sphere
- Same projection \Rightarrow same form factor



Computation of Form Factors

Hemi-Cube Form Factor Algorithm

- Compute form factors for each cell of the hemi-cube (below)
- Store these form factors
- Now find the form factor for every patch P_j relative to A_i

For each face of the hemi-cube:

- i. Clip the scene to the frustum determined by the center of A_i
and the face of the hemi-cube. {Pseudoperspective: frustum→box}
- ii. For each cell of the hemi-cube face
Find the nearest polygon in the scene. {Apply a z -buffer algorithm.}
{Use orthogonal projection after, or perspective projection
before, Pseudoperspective.}
Label each cell with the closest polygon
- iii. For each polygon P_j
Sum the form factors of the cells labeled j

$$F_{di,j} = \sum_{q=j} \Delta F_q$$

Observations

1. Use Reciprocity to Reduce the Amount of Computation
 - $A_i F_{ij} = A_j F_{ji}$
2. Recall the following algorithms
 - Perspective and Pseudoperspective
 - Clipping
 - Z-buffer
3. This computation of form factors takes most of the time.

Form Factors for Hemi-Cube Cells

1. *Area of a Polygon*

$$Area(Polygon) = (1/2) \sum_{j=1}^n |P_j \times P_{j+1}|$$

2. *Point Form Factor*

$$F_{di,j} = \int_{P_j} \frac{\cos \theta \cos \theta'}{\pi r^2} V(x,y) dA_j$$

3. *Point to Cell Form Factor*

$$F_{di,dj} = \frac{\cos \theta \cos \theta'}{\pi r^2} \Delta A_j$$

Form Factors for Hemi-Cube Cells (continued)

4. Top Face (Parallel to Surface -- 8 Fold Symmetry)

- $\cos \theta = \cos \theta' = 1/r$
- $$F_{di,dj} = \frac{\cos \theta \cos \theta'}{\pi r^2} \Delta A_j = \frac{\Delta A_j}{\pi r^4} = \frac{\Delta A_j}{\pi(x^2 + y^2 + 1)^2}$$

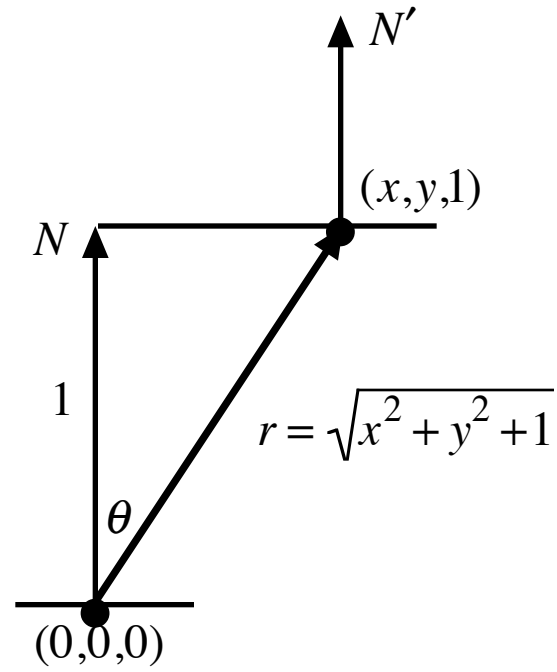
5. Side Face (Parallel to y-axis at $x = \pm 1$ -- 4 Fold Symmetry)

- $\cos \theta = h/r = z/r$ $\cos \theta' = 1/r$
- $$F_{di,dj} = \frac{\cos \theta \cos \theta'}{\pi r^2} \Delta A_j = \frac{h \Delta A_j}{\pi r^4} = \frac{z \Delta A_j}{\pi(y^2 + z^2 + 1)^2}$$

6. Side Face (Parallel to x-axis at $y = \pm 1$ -- 4 Fold Symmetry)

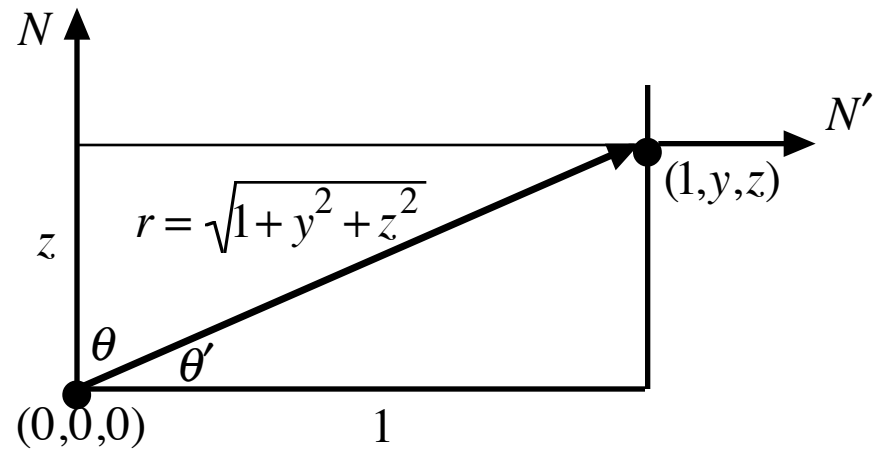
- $\cos \theta = h/r = z/r$ $\cos \theta' = 1/r$
- $$F_{di,dj} = \frac{\cos \theta \cos \theta'}{\pi r^2} \Delta A_j = \frac{h \Delta A_j}{\pi r^4} = \frac{z \Delta A_j}{\pi(x^2 + z^2 + 1)^2}$$

Top Face Parallel to Surface



$$\cos \theta = \cos \theta' = 1/r$$

Side Face Parallel to yz-Plane at $x = \pm 1$



$$\cos \theta = h / r = z / r \quad \cos \theta' = 1 / r$$

Recapitulation

1. *Mesh the Surfaces*

Break each surface into small surface patches

2. *Compute the Form Factors for each pair of surface patches*

Use the hemi-cube algorithm

3*. *Solve the linear system for the radiosities $\{B_i\}$*

$$B_i = E_i + \rho_i \sum_{j=1}^N F_{ij} B_j$$

Must do this computation 3 times, once for each primary (RGB)

4*. *Compute radiosities at the vertices of the patches*

Again do this computation 3 times, once for each primary (RGB)

Recapitulation (continued)

5. Pick a Viewpoint
6. Determine which surfaces are visible
Use any hidden surface algorithm
7. Apply Gouraud shading to the visible surfaces.

Shading

Flat Shading

- Use Calculated Radiosity for Each Patch

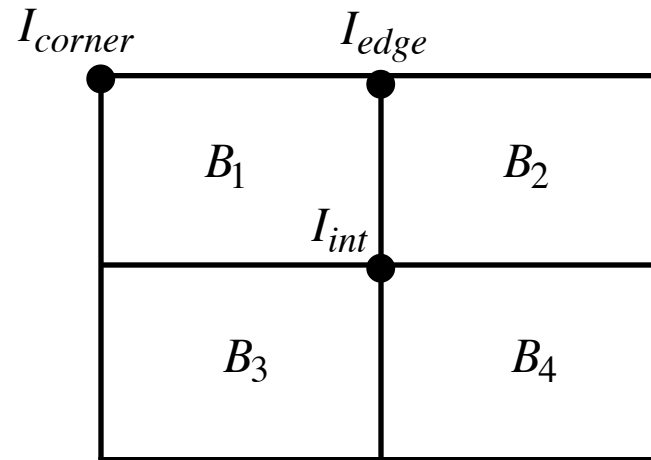
Gouraud Shading -- Regular Mesh

- $I_{\text{int}} = (B_1 + B_2 + B_3 + B_4) / 4$
- $I_{\text{edge}} = (B_1 + B_2) / 2$
- $I_{\text{corn}} = B_1$

or

- $(I_{\text{edge}} + I_{\text{int}}) / 2 = (B_1 + B_2) / 2$
 $\Rightarrow I_{\text{edge}} = B_1 + B_2 - I_{\text{int}} = (3B_1 + 3B_2 - B_3 - B_4) / 4$
- $(I_{\text{corn}} + I_{\text{int}}) / 2 = B_1$
 $\Rightarrow I_{\text{corn}} = (7B_1 - B_2 - B_3 - B_4) / 4$

Gouraud Shading -- Regular Mesh



- $I_{int} = (B_1 + B_2 + B_3 + B_4) / 4$
 - $I_{edge} = (B_1 + B_2) / 2$
 - $I_{corn} = B_1$
- or
- $(I_{edge} + I_{int}) / 2 = (B_1 + B_2) / 2$
 $\Rightarrow I_{edge} = B_1 + B_2 - I_{int} = (3B_1 + 3B_2 - B_3 - B_4) / 4$
 - $(I_{corn} + I_{int}) / 2 = B_1$
 $\Rightarrow I_{corn} = (7B_1 - B_2 - B_3 - B_4) / 4$

The Radiosity System of Linear Equations (N Large)

Individual Equations

$$B_i = E_i + \rho_i \sum_{j=1}^n F_{ij} B_j \Leftrightarrow \sum_{j=1}^n (\delta_{ij} - \rho_i F_{ij}) B_j = E_i$$

System of Equations

$$\begin{aligned} (1 - \rho_1 F_{11}) B_1 - \rho_1 F_{12} B_2 - \cdots - \rho_1 F_{1n} B_n &= E_1 \\ -\rho_2 F_{21} B_1 + (1 - \rho_2 F_{22}) B_2 - \cdots - \rho_2 F_{2n} B_n &= E_2 \\ \vdots & \\ -\rho_n F_{n1} B_1 - \rho_n F_{n2} B_2 - \cdots + (1 - \rho_n F_{nn}) B_n &= E_n \end{aligned}$$

Matrix Form: $M * B = E$

$$\underbrace{\begin{pmatrix} 1 - \rho_1 F_{11} & -\rho_1 F_{12} & \cdots & -\rho_1 F_{1n} \\ -\rho_2 F_{21} & 1 - \rho_2 F_{22} & \cdots & -\rho_2 F_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ -\rho_n F_{n1} & -\rho_n F_{n2} & \cdots & 1 - \rho_n F_{nn} \end{pmatrix}}_M \underbrace{\begin{pmatrix} B_1 \\ B_2 \\ \vdots \\ B_n \end{pmatrix}}_B = \underbrace{\begin{pmatrix} E_1 \\ E_2 \\ \vdots \\ E_n \end{pmatrix}}_E$$

Dictionary

B_i = Radiosity on patch P_i -- identified with intensity -- UNKNOWNNS

E_i = Energy emitted from patch P_i -- USER SPECIFIED
(Uniform in all directions -- Diffuse emitter)

F_{ij} = Form factor -- depends only on geometry -- COMPUTED

ρ_i = Diffuse reflection coefficient for patch P_i -- $0 \leq \rho_i \leq 1$ -- USER SPECIFIED

Gathering

Equations

$$M * B = E$$

$$\sum_{j=1}^n M_{ij} B_j = E_i \Rightarrow B_i = \frac{E_i}{M_{ii}} - \sum_{j \neq i} \frac{M_{ij}}{M_{ii}} B_j \quad (i^{\text{th}} \text{ row})$$

Initial Guess

$$B^0 = \begin{pmatrix} B_1^0 \\ B_2^0 \\ \vdots \\ B_n^0 \end{pmatrix} = \text{initial guess.} \quad \text{Try } B^0 = \begin{pmatrix} E_1 \\ E_2 \\ \vdots \\ E_n \end{pmatrix} \quad \text{or } B^0 = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ 0 \end{pmatrix}.$$

Gathering (continued)

Jacobi Relaxation

$$B_i^p = \frac{E_i}{M_{ii}} - \sum_{j \neq i} \frac{M_{ij}}{M_{ii}} B_j^{p-1} \quad 1 \leq i \leq N$$

Gauss-Seidel Relaxation

$$B_i^p = \frac{E_i}{M_{ii}} - \sum_{j=1}^{i-1} \frac{M_{ij}}{M_{ii}} B_j^p - \sum_{j=i+1}^N \frac{M_{ij}}{M_{ii}} B_j^{p-1} \quad 1 \leq i \leq N$$

Convergence

Diagonally Dominant

- Both methods converge for any initial guess when

$$|M_{ii}| \geq \sum_{j \neq i} |M_{ij}| \quad (\text{diagonally dominant}).$$

- True for us, since form factors sum to 1, and $0 \leq \rho_i < 1$.

$$Ax = b \Leftrightarrow Qx = (Q - A)x + b \Leftrightarrow x = (I - Q^{-1}A)x + Q^{-1}b$$

$$x = \text{fixed point of } T(x) = (I - Q^{-1}A)x + Q^{-1}b$$

Observation

- T is a contractive map when
 - A is diagonally dominant
 - Q is diagonal part of A (*Jacobi*)
 - Q is the lower triangular part of A (*Gauss-Seidel*)

Shooting -- Progressive Refinement

Radiosity Equation

- $$B_i = E_i + \sum_{j=1}^N \rho_i F_{ij} B_j$$

Gathering

- B_i due to $B_j = \rho_i F_{ij} B_j$
- Needs all the form factors for every patch.
- One hemicube \rightarrow one patch radiosity

Shooting

- $A_i F_{ij} = A_j F_{ji}$ (Reciprocity)
- B_j due to $B_i = \rho_j F_{ji} B_i = \rho_j F_{ij} B_i \frac{A_i}{A_j}$
- Need only form factors $\{F_{ij}\}$ for patch P_i to update all patches P_j !
- One hemi-cube at a time.
- One hemicube \rightarrow many patch radiosities

Shooting (continued)

Updates

- $\Delta B_j = (\Delta B_j)_{old} + \rho_j F_{ij} \Delta B_i \frac{A_i}{A_j}$
- $B_j = (B_j)_{old} + \rho_j F_{ij} \Delta B_i \frac{A_i}{A_j}$
- $\Delta B_i = 0$ (*shooting surface*)

Shooting Algorithm

a. Initialization

$$B^0 = \begin{pmatrix} E_1 \\ E_2 \\ \vdots \\ E_n \end{pmatrix} = \Delta B^0$$

b. Select patch P_i for which the total power $A_i \Delta B_i$ is maximal.

c. Compute the form factors $\{F_{ij}\}$ for P_i , using one hemi-cube.

d. Update B_j and ΔB_j for all patches P_j . (Shooting)

e. Display scene using current radiosity values B_j .

f. Go to b.

Ambient Correction

Average Diffuse Reflection

$$\rho_{av} = \frac{\sum_{i=1}^n \rho_i A_i}{\sum_{i=1}^n A_i}$$

Average Reflection

$$R = 1 + \rho_{av} + \rho_{av}^2 + \dots = \frac{1}{1 - \rho_{av}}$$

Average Unshot Radiosity

$$\Delta B_{av} = \frac{\sum_{i=1}^n \Delta B_i A_i}{\sum_{i=1}^n A_i}$$

Ambient (Unshot) Light

$$A = R \Delta B_{av}$$

Ambient Correction (for display only)

$$B_i = B_i + \rho_i A$$

Summary

Advantages

- Photorealism
- Energy Transfer
- Soft Shadows
- Color Bleeding
- View Independence

Disadvantages

- Expensive -- Time and Space
- Must Approximate Curved Surfaces with Polygons (Meshing)
- No Specular Reflections

Enhancements

1. Specular Reflection -- 2 pass algorithm
2. Participating Medium (atmosphere, fog) -- volumes
3. Realistic Light Sources (Sillion p.215)
4. Adaptive Mesh Generation (More Accurate Form Factors -- p. 799)
5. Monte Carlo Integration (ray tracing form factor computation)
6. More Accurate Approximations to Radiosity (not constant on patch)
 - Finite Element Methods
 - Wavelets

Light Sources

Emitters not Reflectors

- $E > 0$ $\rho = 0$

Form Factors

- $F_{ij} = (1/A_i) \int_{P_i} \int_{P_j} \frac{S(\theta) \cos \theta'}{r^2} V(x,y) dA_i dA_j$ (arbitrary source)

- $F_{ij} = \int_{P_j} \frac{S(\theta) \cos \theta'}{r^2} V(x,y) dA_j$ (point source)

$S(\theta) = \text{light distribution}$

$$\int_{\Omega} S(\theta) d\omega = 1$$

Sample Distributions

- $S(\theta) = \cos \theta / \pi$ -- Diffuse
- $S(\theta) = \frac{\cos^n \theta}{n+1}$ -- Spotlight
- $S(\theta) = 1 / 4\pi$ -- Isotropic